

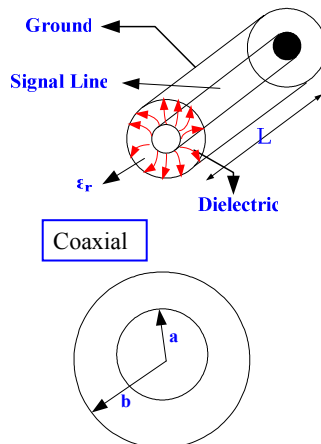
# Transmission Line Geometries

T. Weller  
RF/MW Circuits – I



Powerpoint slides originally prepared by B. Lakshminarayanan.

## Transmission Lines - Coaxial



- Typical:  $1 \leq \epsilon_r \leq 2.2$

- $1\text{mm} \leq b \leq \dots$

- TEM mode:  $Z_0 = \frac{\sqrt{\mu/\epsilon} \ln(b/a)}{2\pi}$

$$V_p = \frac{c}{\sqrt{\epsilon_r}} = \lambda_g f$$

- When dimensions become “electrically large” non-TEM modes can propagate. They are dispersive.

Above “cut-off” frequency ( $f_c$ )

- Keep  $a, b, \epsilon_r$  small for high  $f_c$

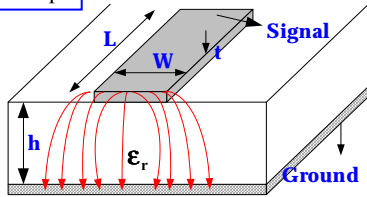
$$f_c = \frac{c \left( \frac{2}{a+b} \right)}{2\pi \sqrt{\epsilon_r}}$$



Department of Electrical Engineering, University of South Florida

## Transmission Lines - Microstrip

Microstrip



- Typical:  $1 \leq \epsilon_r \leq 13.1$ 
  - $0.1\text{mm} \leq h \leq 2.5\text{mm}$
  - $0.5\mu\text{m} \leq h \leq 35\mu\text{m}$   
(100GHz)    (10GHz)
- Microstrip is not a pure TEM mode if  $\epsilon_r \geq 1$  but close to TEM (called quasi-TEM) if  $h \ll \lambda$ .
- Pure TEM exists only in homogeneous medium



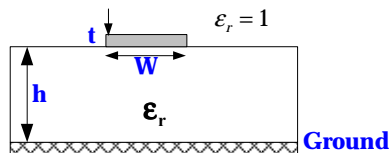
Department of Electrical Engineering, University of South Florida

## Microstrip (cont'd)

- Effective dielectric constant:
  - If microstrip were embedded in a uniform medium and had same  $Z_0$  and  $V_p$  as in non-uniform medium then the equivalent dielectric constant will be  $\epsilon_{re}$

$$\epsilon_{re} = \frac{\epsilon_r + 1}{2} + \text{correction factor}$$

$$V_p = \frac{c}{\sqrt{\epsilon_{re}}}; \quad \beta = \frac{\omega}{V_p} = \frac{2\pi}{\lambda_g} \quad \text{for quasi TEM mode!!!}$$



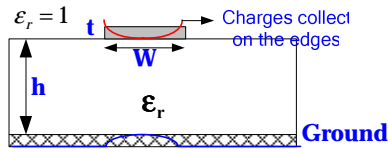
- Equations for  $Z_0$  and  $\epsilon_{re}$  (or  $\epsilon_c$ )  $\Rightarrow$  page 144-145 (Pozar 3<sup>rd</sup> edition). Look in **Transmission Lines and Waveguides** Chapter



Department of Electrical Engineering, University of South Florida

## Microstrip (cont'd)

- Higher order modes:



- When microstrip dimensions become electrically large, higher order modes will propagate ( $f_{c,TE1}, f_{c,TR}$ )

$$f_{c,TE1} = \frac{c}{4h\sqrt{\epsilon_r - 1}} \quad f_{c,TR} = \frac{c}{\sqrt{\epsilon_r}(2W + 0.8h)}$$

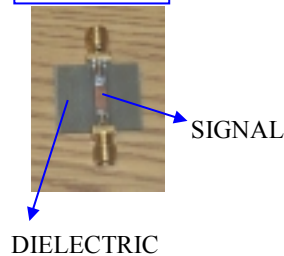
- Keep  $f < f_{c,TE1}$  and  $f_{c,TR}$
- Loss: Conductor, dielectric, and radiation  $\Rightarrow$  all increase with frequency



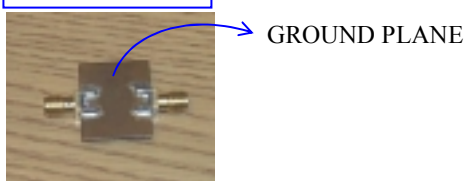
Department of Electrical Engineering, University of South Florida

## Some pictures

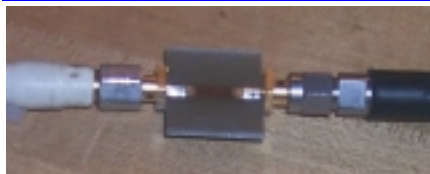
TOP VIEW



BOTTOM VIEW

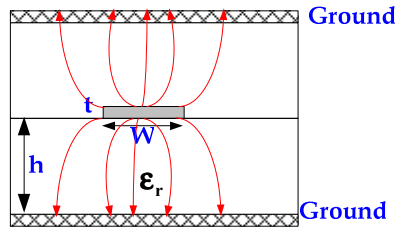


Typical connection for measurement



Department of Electrical Engineering, University of South Florida

## Stripline



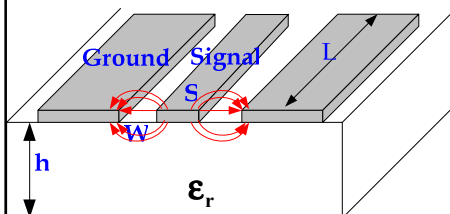
- Homogenous medium  $\Rightarrow$  non-dispersive  
 $\Rightarrow$  TEM mode of propagation

$$V_p = \frac{c}{\sqrt{\epsilon_r}}$$

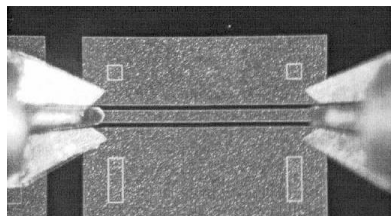


Department of Electrical Engineering, University of South Florida

## Coplanar Waveguide



Coplanar Waveguide (CPW)



TOP VIEW

- Less dispersive than microstrip
- Easy to connect to ground
- $Z_0$  decreases as  $S/(S+2W)$  increases and as  $\epsilon_r$  increases
- Very good for mm-wave design
- To prevent higher order modes propagation, keep

$$S + 2W < \left( \frac{\lambda_g}{10} \right) \quad \epsilon_{re} = \frac{\epsilon_r + 1}{2}$$



Department of Electrical Engineering, University of South Florida